AO/1-9934/19/D/SR Tumbling motion assessment for space debris objects

Final Presentation

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9th of September 2022 Teleconference with ESOC

Outlook

- Introduction
- Attitude models
- IOTA software
- Observation campaign
- Radar observations
- Amplitude method
- Epoch method
- Attitude evolution
- Conclusions

Introduction

- Space debris population growth
- Possible solution: Active Debris Removal
- Knowledge of attitude is necessary
- Current project: development of methods for attitude determination and prediction:
	- Attitude models
	- Attitude determination (amplitude and epoch method)
	- Software for attitude prediction and observation simulations
	- Observations (CCD, photon counter, SLR, radar)
	- Process and product formats and standards

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Attitude models

- Idealized categories
- LEO: stronger influence of gravity gradient and eddy currents
- Eddy currents is stabilizing perturbation
- Satellites have solar panels and SRP is not stabilizing
- MEO/GEO: stronger influence of SRP

Eddy currents

- $\mathbf{M}_{EC} = \left[\mathbb{S} \left(\boldsymbol{\omega} \times \mathbf{B} (\mathbf{v}, \nabla) \mathbf{B} \dot{\mathbf{B}} \right) \right] \times \mathbf{B}.$ • Eddy currents torque
- Dissipative term (Eddy current): $\omega \times B$.
- Related to orbital motion: $\frac{1}{(v,\nabla)B}$ and $\dot{\mathbf{p}}$
- Dissipative terms dominates at first (proportional angular velocity)
- Orbital terms dominate after spin velocity has diminished (in the phase of gravitational capture)
- Orbital terms tend to align momentum vector to orbit normal and stabilize to a momentum depending on the orbit
- Magnetic tensor M: $\vec{T} = (M\vec{\Omega}) \times \vec{B}$.

• E.g. spherical shell

$$
M = \frac{2\pi}{3}\sigma R^4 e \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}
$$

- For flat surfaces computation similar to moment of inertia
- Distribution of conductive material σ

Eddy currents

3 phases:

- Dissipation -> flat spin
- Exponential decay
- Stabilization

 Θ_A angle between angular velocity and major axis of inertia (dissipation phase)

Gravity gradient

- No contribution to energy loss (conservative)
- Big contribution to change of momentum direction
- Ideally, precession of momentum around orbit normal (decay phase)
- E.g. rocket body:

$$
P_{g} = \frac{2\pi^{2}I_{0}r^{3}}{GM_{e}\Delta IP_{rot}\cos\theta}
$$

- Not ideal precession due to orbit precession:
- With low spin rate (gravitational capture phase):
	- => alignment to orbit normal
- Oscillations during capture, motion like a pendulum

Eddy current + grav. grad.

 θ_H angle between angular momentum and normal to orbital plane

Gravitational capture:

- Angular rotation low
- Gravity gradient bigger than eddy currents
- => gravity gradient aligns momentum vector to orbit normal
- => Spin-orbit resonance (mostly 1:1, but depends on orbit)

Solar Radiation Pressure

- No magnetic dissipation effect
- Spin rate constant or changes due to SRP
- Mostly S/C with large illuminated surfaces
- Increase/decrease spin rate:
	- Asymmetric solar panels
	- Offset of center of mass w.r.t. figure
- Cyclic and secular trends

Simulation: wind wheel

- Wind wheel, rotation around x axis
- Sun illumination parallel to $x =$ torque along x
- Sun illumination in x-y plane => partial torque along x, no torque with Sun parallel to y
- Simulations:
	- Polar orbit, 36'000 km altitude
	- Moments of inertia are 3×10^3 , 3×10^3 , 1×10^3 kg m²
	- $-$ Box (2 x 2 x 2 m), wings (1 x 2 m)
	- 10° canting angle

Periodic pattern

• Initial rotation

=> stabilize the direction of angular velocity => throughout the year Sun illuminates front/back of wheel => increase/decrease: yearly period

- Different front/back reflection coefficient => increase/decrease stronger in the first half of year
	- => secular slope

Pseudo periodicity

- No initial velocity + different front/back coeff.
	- => secular + periodic trend
	- => pseudo periodic (chaotic)
- Same results with only 1 wing

Monotonic trend

• 1 wing with no canting => monotonic trend (radiometer) => or almost static attitude (wind vane)

Different behaviours

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Amplitude method

- Method proposed by V. Williams (1979)
- Determination of the spin axis orientation
- Cylindrical elongated objects: R/B
- Stable attitude state (flat spin)
- Diffuse reflection of Sun light
- No reflection on top/bottom of cylinder
- Constant spin axis during one observation passage
- Constant spin axis over time period of several observations

Amplitude method

- Brightness ratio (BR): $M_{max} M_{min} = -2.5 \log_{10} \frac{J_{max}}{I_{max}}$ J_{min}
- Ratio depends on direction of spin axis
- For given Sun/observer direction and brightness ratio => there is a set of solutions
- More ratios are necessary for a unique solution

Amplitude method

- Measurement of brightness ratio from light curve.
- Determination of the celestial coordinates of satellite, Sun, observer.
- Calculation of the phase angle.
- Construction of the satellite coordinate system
- Numerical search of tumble axis directions comparing measured and simulated brightness ratios.
- Conversion of tumble axis directions in celestial coordinates.
- Iteration of the previous steps for at least three different observation geometries of the same object.

Amplitude method: CZ-3B R/B

Amplitude method: CZ-3B R/B

- Solution regions for 3 light curves
- Intersection shows spin axis direction
- Script identifies region of overlapping

Simulated light curves: CZ-3B R/B

- IOTA simulations at 3 obs. epochs
- Top/bottom absorption coeff. = 1
- Rotation axis (RA 235.2°, DEC 64.1°)
- Brightness ratios from obs.: -3.1, -2.8, -2.4
- Simulated brightness ratios: -3.1, -2.3, -2.0
- Possible divergence due to shape/reflection model

Solution evaluation

- Graphical intersection shows that in principle there is a solution
- Although unlikely, it can be that intersection shows not the real spin axis
- If assumption not fulfilled, error exceeds the formal value given by measurement noise
- If spin axis not constant, solution is kind of an average orientation
- Simulations for the above case CZ-3B R/B on GTO orbit:
	- Time interval of 3 observations is about 2 months
	- Gravity gradient torque causes precession of spin axis
	- Spin axis might change orientation of 30° within 2 months
- Ideally for low orbits: observation series within few days

Simulated light curves: Envisat

- Validation of IOTA simulated light curves
- Availability of quite accurate Envisat attitude state in the past
- Joint CMOS-SLR-Radar campaign 21.09.2016 (previous ESA Attitude project)

Simulated light curves: Envisat

- Violet: observed light curve
- Black: one material
- Blue: nominal material reflection coeff.
- Violet: observed light curve
- Blue: modified material reflection coeff.

Simulated light curves: Envisat

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Method of Yanagisawa et al.

- Simple formulation for ellipsoid, function of θ
- α phase angle, M optic coeff.

$$
A = (1 + M\alpha)A_0 \qquad A_0 = \frac{a\sqrt{b^2\cos^2\theta + c^2\sin^2\theta}}{b\sqrt{a^2\cos^2\theta + c^2\sin^2\theta}}
$$

For cylinder:

$$
A_0 = 1/(\cos\theta + \frac{\pi}{4}Rd\sin\theta)
$$

- d diameter divided by length
- R albedo of bottom/top divided by side albedo
- Solution as least squares problem
- At least as many observations as parameters
- Precession parameters can be estimated

Precession

$$
A_0 = 1/(\cos\theta + \frac{\pi}{4}Rd\sin\theta)
$$

$$
R.A. = RA_0 + D \sin(2\pi t/T + \beta) / \cos(Dec.)
$$

Dec. = Dec₀ + D cos(2\pi t/T + \beta)

$$
l = \cos(R.A.) \cos(Dec.)
$$

$$
m = \sin(R.A.) \cos(Dec.)
$$

$$
n = \sin(Dec.)
$$

- RA_0 Dec₀ (precession axis)
- RA, Dec (rot. axis)
- Approximation for small D
- For larger D it is more complicated (e.g. Rodrigues rotation formula)
- Additional estimated parameters:
	- RA_0 DEC₀
	- D (precession angle), T (precession period), β (phase)

LSQ convergence

- Loss function vs RA/DEC of spin axis
- Tests with all precession parameters show low reliability
- Use several starting points (multiple local minima)
- Tests w/o precession parameters show reproducible results (different LSQ start points with same result).
- However, high residuals
- Problem of Yanagisawa model?

Comparison with Williams

- Yanagisawa depends on phase angle through an empirical formula: $(1 + M\alpha)$
- But it does not depend on the absolute direction of Sun and of the spin axis
- Compare with Williams, no top/bottom reflection (R=0) =>
- $\frac{F_{min}}{F} =$ F_{max} $|\cos \theta|$ $1+M\alpha$

 \Rightarrow Yanagisawa model: approximation for θ close to 90°

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Attitude evolution

- Compare IOTA simulations with literature results
- Orbit: 800 km, inclination 70°, angular velocity 1 rad/s
- Only effect of Eddy currents
- Exponential damping and stabilization
- Angle θ_A betw. angular velocity and axis of maximum inertia => flat spin
- Eddy currents: transition phase (typical bend) after 1 year
- $I = 5 \times 10^3$ kg m², M = 2 x 10⁵ S m⁴, B = 40'000 nT

$$
=
$$
 Decay rate $\tau \approx \frac{I}{M B_{\perp}^2} \approx 2.2 \text{ yr}^{-1}$

Attitude evolution

- Combined effect of eddy currents and gravity gradient
- Initial angular velocity 0.5°/s
- Precession of angular moment, phase φ_I relates to projection angular momentum onto the orbital plane
- P_{rot} = 60 s, orbit at 600 km altitude, ratio $\frac{I_0}{I_0 I_3}$ \approx 1.28, and θ = 70°

•
$$
P_g = \frac{2\pi^2 I_0 r^3}{\mu (I_0 - I_3) P_{rot} cos\theta} \approx 2
$$
 weeks

- Stabilization with gravity gradient torque
- Orbital resonance 1:1, angular velocity 0.06°/s
- Oscillation of angular velocity (capture phase) $\omega_g = \frac{1}{2}$ $2\mu(I_0-I_3)$ I_0r^3

 \approx 1.3 h

Attitude evolution

- IOTA with only Solar Radiation Pressure considered
- Box (2 x 2 x 2 m), wings (1 x 2 m), 10° canting angle, polar orbit
- Simulation with different front/back panel properties
- Annual variation with secular slope of 0.02 rad/s
- Earth radiation force and penumbra with LEO at 800 km
- Surface of 8 $m^2 \approx 10^{-5}$ N expected
- Penumbra time in LEO about 10s

Spin rate evolution: CZ-3B R/B

- Combination of observations from Graz, Zimmerwald, TIRA
- Evolution of spin rate determined for several objects
- Check the consistency of the extracted periods
- Example: CZ-3B rocket body (2019-090D) => $\tau \approx \frac{I}{M}$ MB_\perp^2
- IOTA simulation: consider real distribution of Earth magnetic field

- Violet: Graz photon counter
- Red: TIRA, Blue: Zimmerwald
- Spin rate from fit: 0.24 yr⁻¹
- Consider: $CZ-3B \sim$ Ariane 4 H10
- Refined values: $35'000$ km m², 4 x 10^6 S m⁴
- Simulation gives: \approx 0.2 yr⁻¹

Spin rate evolution: Jason-2

- Low effect of damping eddy currents, 1300 km altitude
- Solar panels \Rightarrow effect of SRP
- From SLR, radar: spin axis approx. perpendicular to orbit plane
- From radar: solar panels almost orthogonal
- Different reflection coeff. for front/back side of panels

- Violet: Graz photon counter
- Green: Graz SLR
- Red: TIRA, Blue: Zimmerwald
- Spin rate increase, not regular pattern
- Low angular velocity does not keep attitude stable
- Wind wheel model not applicable
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Conclusions

- Development of attitude models, attitude determination methods, simulation s/w
- Attitude determination: amplitude method
	- Method of Williams: spin axis orientation of R/B can be determined with 3 or more observations
	- Accuracy from few to tens of degrees
	- Some assumption, e.g. constant spin axis during observations interval, strongly influence the accuracy
	- Method of Yanagisawa uses approximate model and can be used only in a limited range of observation geometries
- Attitude determination: epoch method
	- Characterization of the limits and required spin period accuracy
	- => Improvement of preprocessing for period extraction. Savitzky-Golay on local data samples for successful detrended time derivative series
	- Apparent motion is a limiting factor: in GEO too small
	- In LEO enough apparent motion, but accuracy limits a significant prediction of spin orientation
- Attitude simulation software and evolution models
	- Simulation of light curves for objects with different materials (Envisat, R/B)
	- Simulation of attitude evolution under the effect of eddy currents, gravity gradient, solar radiation
	- Prediction of spin rate for R/B
	- Large amount of observations, more than 20 objects, over 2 and more years, spin periods and trends
- Definition of new process and product formats and standards

Tumbling motion assessment for space debris objects

Final presentation

September 9, 2022

Tumbling motion assessment for space debris objects Final Presentation, 2022-09-09

- Major tasks
	- \triangleright Pre-computed coefficients
	- \triangleright Magnetic tensor model
	- \triangleright Earth radiation model
	- \triangleright IOTA GUI simulation manager and simulation setup
- Minor tasks
	- \triangleright S/C geometry surface reflectivity
	- \triangleright Dynamic solar activity for the aerodynamics model
	- \triangleright Geometry handling optimization
	- \triangleright TLE import via CSTATE
	- \triangleright Earth shadow penumbra region
	- \triangleright Generic attitude damping function
	- \triangleright Space-based observer
	- \triangleright Thermosphere wind model (HWM14)
	- \triangleright Output extension: Sun direction, along-track, and radial vectors [and torque vectors as debug output]

Magnetic tensor model

M~ Magnetic tensor \bar{B} ~ Magnetic field $\overline{\omega}$ Angular velocity

Illumination of Earth surface with acceleration due to ERP and SRP

IOTA GUI simulation manager and simulation setup

Browse

pitch [°] 180.000 pitch velocity [%] 0.000 yaw [*] 0.000 yaw velocity [°/s] 0.000

Save Save As Cancel

IOTA GUI result view

- **General**
	- \triangleright Uncertainty Quantification via MC for simulation input (similar to SCARAB4)
	- \triangleright pyIOTA Python wrapper (similar to pyDRAMA/pyMASTER)
	- \triangleright Write full precision snapshots to allow continuation of a simulation
		- Recover from a crash or continue with modified settings
- Models and methods
	- \triangleright Extend eddy current damping for slow tumbling objects (DD-0002 Eq. 6)
	- \triangleright Parallelisation of the coefficient DB calculation
	- \triangleright Rotating S/C parts, e.g. solar arrays (similar to DMF-03)
	- \triangleright Use pre-computed coefficients for light curve generation (similar to DMF-05)
	- \triangleright Improve RCS model (similar to DMF-05, model TBD)
	- \triangleright Implement MIRAD micro-particle impact model
	- Ø Consider YORP effect

Thank you for listening

Any questions?

TUMBLING MOTION ASSESSMENT FOR SPACE DEBRIS OBJECTS

ESA AO/1-9934/19/D/SR Monthly Meeting 13

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OBSERVATION CAMPAIGN OVERVIEW

- 1) Historic data: 2018-2020, especially from former ILRS targets
- 2) Pre selection campain 2020: analysing current rotation behavior and "quality" of light curves
- 3) Based on 2): reduction of target catalog to "object of interest" catalog: 26 targets
- 4) Graz extensive observation campaign of 26 targets mainly performed in 2021
- 5) Few targets selected for joint tracking campain with different sensors

OBJECTS OF INTEREST LARGE LIST

GRAZ LARGE CAMPAIGN STATISTICS

Graz campaign data summary including historic data

- \cdot 2018 2022
- Data uploaded on servers
- Light curves from all of the large catalog targets
- Best tracking coverage: Jason 2 -> ~ 200 LC + 600 SLR passes

STATISTICS 2018

Historic data: mainly

• Envisat, Jason-2, ERS-2, 2 Glonass satellites

STATISTICS 2019

Historic data: mainly

• Envisat, Jason-2, ERS-2, 2 Glonass satellites

2019: Graz priority target: Tracking statistics
LC: 47, SLR: 278, SDLR: 14

7

STATISTICS 2020

Historic data: mainly

• Envisat, Jason-2, ERS-2, 2 Glonass satellites

2020: Graz priority target: Tracking statistics
LC: 75, SLR: 41, SDLR: 22

STATISTICS 2021

Observation campaign

- Mainly SLR + LC
- 421 light curves, 102 SLR, 24 SDLR

2021: Graz priority target: Tracking statistics
LC: 421, SLR: 102, SDLR: 24

STATISTICS 2022

Some targets still monitored by IWF

• Jason-2, Envisat

JOINT TRACKING CAMPAIGN

Selected targets:

- Jason-2
- Envisat
- SL-16 rocket body

Summary:

- Observation sessions including one TIRA pass, maximum 24 hours / session
- Each session: Graz, Zimmerwald collects data of all possible passes, TIRA collects one radar pass
- Simulaneous tracking not necessary but welcome
- Observation schedules were distributed to partners

JOINT TRACKING CAMPAIGN

Preferred observation characteristics: sensor

! DANKE FÜR IHRE AUFMERKSAMKEIT !

Tracking and Imaging Radar (TIRA)

Different kinds of measurements for attitude motion estimation

 RCS curve (L-band tracking radar) RTI plot (Ku-band imaging radar) **Series of ISAR images (Ku-band imaging radar) Estimation of the velocity vector (angular velocity and spin** axis) and of the initial state through a ML approach **Applicability** Slow tumbling objects (to avoid under-sampling issues in the ISAR images) Assumes a constant rotational velocity vector during the observation time (or at least a part of it)Fraunhofer Page 6 01.09.2022 © Fraunhofer FHR **Open**

Estimation of the attitude motion of space objects

Ku-band imaging radar

Conducted measurements

L-band tracking radar and Ku-band imaging radar

- TRKI (13.10): 02009a, 27386, Envisat
- TRKI (12.11): 02009a, 27386, Envisat
- TRKI (13.10): 08032a, 33105, Jason-2
- TRKI (29.10): 19063b, 44548, R/B CZ-2D
- TRK (12.11): 19090d, 44867, R/B CZ-3B (no imaging data)
- TRKI (23.11): 00008c, 26083, Globalstar M060

Conducted measurements

TRKI (13.10 / 12.11): Envisat

- RTI plot
	- **Time between two nodes is approximately 110 s**
	- Object rotates around 180 deg during this time
	- Apparent angular velocity is around 1.6 deg/s
- **ISAR image series and WGM**

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- The best match is achieved with the rotational velocity vector [0.5; 1.07; 1.2] deg/s (ECI J2000); estimated angular velocity: 1.68 deg/s
- Decreasing match with the projected WGM towards the end of the passage
- \blacksquare Complex tumbling motion, assumption of consta rotational velocity vector is not fulfilled

Conducted measurements TRKI (13.10): Jason-2

- **L**-band signature
	- Complex tumbling object, no clear periodicity could be observed
- **ISAR** image
	- No external damage could be observed
	- Solar panel planes appear to be orthogonal to each other
	- The image was produced assuming a rotational velocity of 9 deg/s about an axis orthogonal to the orbit plane. In the inertial system the assumed rotational velocity vector is [-5.5; 6.1; -3.7] deg/s (ECI J2000)
	- The cross-range scaling of the image confirms this assumption
- RTI plot
	- Apparent angular velocity is around 9 deg/s

Fraunhofer

Measured RCS, Object: 26083, Observation: 23.11.2021

600 800 Relative time [s]

Conducted measurements

TRKI (23.11): Globalstar M060

dRem

200

- **L**-band signature
	- **Fast tumbling object with complex motion**
	- Region 1, t<600s, apparent rotational velocity ~6.8 deg/s
	- Region 2, t>600s, apparent rotational velocity ~13 deg/s
- ISAR image
	- **Undersampling in the cross-range direction causes aliasing**
	- The image was produced at relative time 480 s assuming a rotational velocity of 6 deg/s with rotation axis orthogonal to the orbit plane ([-4.7; -0.8; -3.7] deg/s, ECI J2000)
- RTI plot
	- Very faint maximal range spans at approx. 448 s and 508 s lead to an apparent rotational velocity of 6 deg/s confirming the order of magnitude of the L-band result

Open

1200

Tumbling Motion Assessment for Space Debris Objects

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Environmental characteristics

The selection process of objects-of-interest was based on environmental characteristics analysis.

Estimation of the environmental forces and torques is not exactly possible without knowing how an artificial object interacts with the external factors, but we can characterize environmental phenomena that lead to and affect the tumbling motion.

The environmental forces and torques can be divided into separate categories:

1. Monopolar gravitational field, the force vector changes once per orbital revolution.

2. Bipolar magnetic field, force vector changes twice per revolution.

3. Directional

solar irradiation flux, charged particle flux, residual atmospheric particles. The flux direction can change periodically.

Environmental characteristics

Periodical effects on spinning Jason-2

- Use TLE to simulate orbital configuration at constant time step (0.1 day)
- Apply FFT for identification of the periodical signals in the simulated time series
- The change of the orbital configuration wrt the Sun stimulates tumbling motion

All ~300 objects-of-interest is processed and characterized in terms of expected periodicity in the tumbling motion due to the changes in the orbital configuration.

Satellite attitude observation

High rate laser and optical tracking allows for accurate attitude measurement of the active and passive satellites.

Graz SLR station simultaneously performs laser ranging and light curve measurements (since 2015).

The hypertemporal light curves measured at the single photon resolution present a high level of details due to the fact that the photon counters do not integrate the incoming optical signal (as opposed to the CCD technology).

The high-rate SLR allows for the mm-accuracy absolute range measurements that reveal motion of the individual corner cube retroreflectors wrt the satellite CoM.

The pattern of the data distribution depends on:

- LC: the angular configuration Sun-Satellite-Observer

- SLR: the range between the Satellite and Observer optical reflection and reference points

M. Steindorfer

Tumbling Motion Observation - Data Analysis Sheet. Graz, 18 May 2020, 19:33:17

6 6

Tumbling Motion Observation - Data Analysis Sheet. MMT, 24 October 2019, 2:10:54

Object: NOAA 3

Orb. period: 1.9 h

Object age: 46.0 y

RCS: 2.5 m2

 -6.5

 -70

 -7.5

 -8.0

 $-8.$

1.00

 $\frac{6}{2}$
 $\frac{0.75}{0.25}$
 $\frac{0.50}{0.25}$

 0.00

 -6.5

 -7.0

 -7.5

 -8.5

 Ω

90

180

Spin phase [°]

270

360

 -1.50

25.339

Period [s]

 $+1.50$

Reversed StdMag

 0.0

Reversed StdMag

NORAD: 6920

Pass information Duration: 1m:38s Data points: 1243 Sampling rate: 10.0 Hz

Closest approach Topo el: 81.0° Slant range: 1529 km Phase angle: 58.7° Sim. app. mag.: 6.3 Solar Beta angle: 60.7°

360

270

 -1.50

25.959

Period [s]

 $+1.50$

180

Spin phase [°]

90

 Ω

Tumbling Motion Observation - Data Analysis Sheet. MMT, 9 November 2020, 1:54:17

Topocentric

 0^o

 30°

 60°

 $\frac{1}{90^{\circ}}$

 180°

Description of rotation Spin vector definition

Rotational motion of a rigid object about its center of mass can be characterized by the spin angular momentum vector L oriented in an external, right-handed Cartesian coordinate system \mathbb{R}^3 about which the body spins in a counter-clockwise direction at an angular rate equal to the magnitude of L .

During an overhead pass of a satellite above a ground tracking system, it is possible to predict an inertial, satellite-centered unit direction vector \hat{T} toward the telescope. Transformation of \hat{T} from an external \mathbb{R}^3 $(\hat{T}_{\mathbb{R}^3})$ to a spacecraft body-centered and -fixed coordinate system (BCS) can be realized by $\hat{T}_{BCS} = A\hat{T}_{\mathbb{R}^3}$, where the attitude tensor A between the external and the embedded reference frames is a rotation matrix computed by:

$$
A = R_2(-x_P)R_1(-y_P)R_3(\gamma)R_1(\frac{\pi}{2} - \delta)R_3(\frac{\pi}{2} + \alpha)
$$

where the \mathbf{R}_1 , \mathbf{R}_2 and \mathbf{R}_3 are the standard rotation matrices about the x, y and z-axis respectively.

Description of rotation Spin vector definition

The orientation of L in ℝ³ ($L_{\mathbb{R}^3}$) is defined by spherical angles α , δ corresponding to right ascension and declination in the case of Earth Centered Inertial reference frame (ECI, J2000) being an external system.

Rotation angle γ increases at the rate of $\omega = ||L||$, while the pole coordinates x_P and y_P describe the relative position of L with respect to the satellite body axis $+Z_{BCS}$. In this work we assume that the body's pole axis coincides with the axis of rotation, thus x_p and y_p are 0.

For a given spin vector $L_{\mathbb{R}^3}$ it is possible to find the relative orientation of \hat{T}_L (satellite-centered observer direction vector) by:

$$
\widehat{T}_L = R_1 \left(\frac{\pi}{2} - \delta \right) R_3 \left(\frac{\pi}{2} + \alpha \right) \widehat{T}_{\mathbb{R}^3}
$$

where the azimuthal motion of \hat{T}_L about L during a satellite pass is known as an apparent rotation effect.

Timeseries analysis – epoch methods

Several methods can support high level of automation of the tumbling motion determination processes:

- Savitzky-Golay filters for timeseries approximation, detrending with time derivatives.
- Spectral analysis $(Lomb)$ for apparent rate determination.
- Phase Dispersion Minimization for apparent and inertial periodicity determination.
- Autocorrelation for apparent periodicity.
- Inertial PDM mapping for spin vector orientation.

Apparent PDM

Typical, apparent periodicity as seen by the observer.

The phase coordinate of a data point is computed as a fraction of a fixed (tested) period.

Inertial PDM

Based on the attitude tensor transformation.

The phase coordinate of a data point is derived through the inertial-to-body transformation of a satellitecentered phase vector. The body-fixed azimuth of the transformed phase vector is the phase coordinate of the observed data point.

This method requires modelling a time-dependent, satellite attitude tensor that takes the satellite spin vector \overline{L} as an input. Optimization of \overline{L} (orientation and magnitude) minimizes dispersion of the folded pattern (measured by the variance ratio Θ).

 90°

Apparent and Inertial Phase Folding – **Lightcurve**

CNES

Apparent and Inertial Phase Folding – **SLR**

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Approximated data, with 3° moving polynomial fit (SGF). Polynomial window 3 s, step 0.1s; Orthogonal polynomial fit (Gram method).

The profile of the solution line allows finding the statistical parameters of the dominant signal:

- Full Width at Half-Maximum (FWHM) of the solution line represents the errors and inaccuracies of the analysis related to the sampling noise or apparent rotation and frequency shift effects.
- Signal-to-Noise Ratio (SNR). Assuming Gaussian distribution of the solution (f_{max}) error it is possible to calculate its standard deviation as $\sigma = \frac{FWHM}{2\sqrt{\ln(4)}}$ and $SNR = \frac{f_{max}}{\sigma}$. Here, the standard deviation represents the noise and other negative interference to the measured signal.
- 14 - Coefficient of Variation (CoVar) measures relative variability and is defined as the standard deviation divided by the mean, multiplied by 100 %: $\text{Cov}ar = \frac{\sigma}{f_{max}} \cdot 100\%.$

Comparison of Lomb and PDM on approximated and derivative timeseries (Jason-2 lightcurve)

Timeseries analysis, Jason-2 **light curve**

Apparent vs. Inertial PDM

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 -30°

IWF.OEAW.AC.AT

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Timeseries analysis, TOPEX **SLR**

Apparent vs. Inertial PDM

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Results of the epoch methods

DMSP 5 D-2 SATELLITE

Approximated data: 2-a,b, 4-a,b,c Time derivative: 3-a,b, 5-a,b,c

18123

23205

NASDA (JAXA)

Approximated data: 2-a,b, 4-a,b,c Time derivative: 3-a,b, 5-a,b,c

40000

30000

25000

20000

15000

35000

30000

25000

20000

 $40 20₁$

 -20

 $1.0₁$

 0.5

 $0₀$

 -1.0

 $1.0 -$

 $0.0₁$ com

 -1.0

 $\frac{9}{24}$ -0.5

 $\mathop{\rm coeff}$ $0.5 -$

 $\mathop{\rm coeff}\nolimits$

 $_{\rm corr.}$

 $rac{9}{22}$ -0.5

Photon count rate 1° der. [kHz/s]

 $\frac{1}{2}$ 35000

270

270

 -0.25 4.867 $+0.25$

Periodicity [s]

 -0.25 4.868 $+0.25$

Periodicity [s]

360

360

Solution profile

Theta: 0.241

Period: 4.867 s

FWHM: 0.054 s

StdDev: 0.023 s

CoVar: 0.474 %

Solution profile

Period: 4.868 s

FWHM: 0.049 s

StdDev: 0.021 s

CoVar: 0.429 %

SNR: 233.0

Theta: 0.394

SNR: 211.1

Approximated data: 2-a,b, 4-a,b,c Time derivative: 3-a,b, 5-a,b,c

33105

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Results of the epoch methods

270

270

 $0⁸$

 0.6

 0.4

 0.2

 $0₀$

 0.8

 0.6

 0.4

 0.2

 $0₀$

 -1.50 24.069 $+1.50$

Periodicity [s]

 -1.50 24.061 $+1.50$

Periodicity [s]

É

å

360

360

Solution profile

StdDev: 0.154 s

Solution profile

Theta: 0.620

StdDev: 0.102 s

SNR: 235.2

SNR: 156.7

Theta: 0.293

Approximated data: 2-a,b, 4-a,b,c Time derivative: 3-a,b, 5-a,b,c

Frequency line

Frequency analysis

Frequency: 0.048 Hz

FWHM: 3.474 mHz

StdDev: 1.475 mHz

Frequency analysis

Frequency: 0.048 Hz

FWHM: 3.459 mHz

StdDev: 1.469 mHz

Solution profile

Power: 4072.6

Period: 20.767 s

SNR: 32.8

 $0.048 + 0.01$

CoVar: 3.051 %

CoVar: 3.067 %

Solution profile

Power: 7037.0

Period: 20.784 s

SNR: 32.6

rate [MHz]

rate $\left[\mathrm{MHz}\right]$

å

rate 1° der. $[\mathrm{MHz/s}]$ $\overline{2}$

Pho

 coeff 0.5

 R_{1}^{10} (control)

 -1.0

 $1.0 -$

 $\bigoplus_{\substack{0 \leq x \\ y \in \mathbb{R}}} 0.5$

 R_{H}^{0} (compose)

 -1.0

 θ

 $\overline{2}$

 $1.0 -$

25407

360

360

Solution profile

Theta: 0.100

Period: 59.777 s

FWHM: 3.260 s

StdDev: 1.384 s

CoVar: 2.316 %

Solution profile

Theta: $0.716\,$

Period: 59.778 s

FWHM: 0.933 s

StdDev: 0.396 s

CoVar: 0.663 %

SNR: 150.9

SNR: 43.2

Approximated data: 2-a,b, 4-a,b,c Time derivative: 3-a,b, 5-a,b,c

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 $\mathop{\rm int\,rate}$ [kHz]

Phote

Photon count rate 1° der. [kHz/s]

 $\mathop{\rm coeff}$

(com.

 $\rm Rho$

44867

Data fusion

Observed spin period of Jason-2 determined with epoch analysis of Graz single-photon light curves (blue dot) and SLR data (green dot). Appendix C presents example analysis.

Fusion polynomial fit to light curve and SLR data with 95% confidence limits. A 3-degree weighted polynomial fit is constructed with fused spin period data from light curves and SLR observations of Jason-2.

Data fusion

Jason-2 light curve (a1) and SLR (a2) data measured by Graz on 18 May, 2020.

Plots b1, b2 - present results of the inertial phase-folding applied to the respective time series.

Red and blue dots represent location of the positive and negative orbit normal vectors; a blue curve is a satellite orbital plane on the inertial sphere).

Conclusions

- The tumbling motion determination processes can be efficiently performed with a set of epoch methods that extract frequency and periodicity spectra from the observational data,
- this, however, requires an initial data treatment with Savitzky-Golay Filters (SGF) that have powerful denoising and detrending properties, but come at high computational cost.
- The spin vector orientation determination with the epoch methods can deliver only approximate results – a range of possible solutions in a given coordinate system.
- During this project we have identified several areas where more research could lead to a higher level of automation of the tumbling motion determination (multi-pass analysis, variable degree of SGF).

Danke für Ihre Aufmerksamkeit !

