Low Straylight Diffraction Grating (LSG) Final Presentation

30.01.2023, ESTEC Noordwijk

Agenda

13:00 – 13:50	Welcome at ESTEC and Lunch
14:00 – 14:15	Introductory talk
14:15 – 14:45	Measurement and Characterization
14:45 – 15:15	Final Presentation for binary Littrow gratings (SFT2)
15:15 – 15:45	Final Presentation for Echelle gratings (SFT1)
15:45 – 16:00	Coffee break
16:00 – 16:30	Final Presentation for SPDT blaze grating (SFT3)
16:30 – 17:00	Perspectives
17:00 – 17:30	Conclusion and Discussion



Scope of the project

Context

- In spectrometric instruments gratings are a main contributor of straylight
- Straylight in gratings is poorly understood and astonishing straylight phenomena were observed (level and distribution of straylight)
- Origins are manifold and strongly depent on fabrication technology
- Grating design plays an important role and suitable modelling and analysis of straylight is welcomed
- The individual causes of straylight shall be investigated and appropriate changes of the manufacturing process(es) for lower straylight shall be derived

→Short Introduction on straylight measurement





ALBATROSS: 3D-Arrangement for Laser Based Transmittance, Reflectance, and Optical Scatter MeaSurement



- High dynamic range and linearity (> 15 orders of magnitude)
- Sample curvature compensation
- Spectral range: 193 nm 10.6 μm
- 18 motorized axis / degrees of freedom
- Measurements at 633 nm and 10.6 μm

Light scattering characterization of Three-Mirror Anastigmat, TMA





Light scattering quantities



- $\theta_{\rm s/r}$... polar scattering angle
- $\varphi_{\rm s/r}$... azimuthal scatter angle
- $P_{\rm s}$... scattered light power
- *P*_i ... incident light power
- $P_{\rm r}$... specularly reflected light power
- P_n ... diffracted light power
- P_t ... specularly transmitted light power
- $\Delta\Omega_{s}\ \ldots$ detector solid angle

Angle Resolved Scattering (ASTM E2387, ISO19986)

$$\operatorname{ARS}(\theta_i, \theta_s, \varphi_s) = \frac{\Delta P_s(\theta_i, \theta_s, \varphi_s)}{\Delta \Omega_s P_i}$$

Angle Resolved Efficiency

$$ARE(\theta_i, \theta_s) = \frac{P_n(\theta_i, \theta_s)}{P_i}$$

Total scattering (ISO13696)

$$TS = \int_{0}^{2\pi} \int_{2^{\circ}}^{85^{\circ}} ARS \sin \theta_s \, d\theta_s d\varphi_s$$

- Scattering loss
- Energy balance: $100\% = R + T + A + TS_b + TS_f$

Encircled energy

$$S(\theta_r) = \int_{0}^{2\pi} \int_{0}^{85^{\circ}} \operatorname{ARS}(\theta_s, \varphi_s) H\left(\theta_r - \arccos\left[\cos\theta_s \cos\theta_b + \sin\theta_s \sin\theta_i \cos\varphi_s\right]\right) \sin\theta_s d\theta_s d\varphi_s d\varphi_s$$

$$H_{\dots} \text{ Heavisside function}$$

- Scattering in a cone with opening angle θ_r around the different diffraction orders





Fraunhofer

Project approach to address SOW – structural feature types (SFT)





Scattering Footprints of SFTs



- Diffraction efficiency, Scattering loss, Ghost efficiency, analysis of diffraction plane
- Characteristic footprint + topography cross correlation \rightarrow fabrication optimization



Difference between ARS and ARE



- + Diffuse contributions are ideally described with the help of the ARS in order to circumvent the impact of the actual detector geometry /ray-set density in straylight simulations
- Description of isolated peaks (regular and ghost diffraction orders) critically depends on detector geometry



Peak intensities do not depend on detector geometry

polar scattering angle, θ s (°)

-46

-44

- → Important: detector aperture needs to be larger than diffraction peak + oversampling
- Background scattering is not well described

-48

1E-07

1E-08

-50



-40

-42

Topography analysis



- Analysis of long ranging waviness to small lateral features
- For correlation between fabrication imperfections and light scattering

